

MEASUREMENT OF VACUUM SUCTION FORCE ON DIVERSELY CONFIGURED VERTICAL OUTER WALLS OF BUILDINGS

Young-Bog Ham¹, Byung-Ju Lim^{1*}, Chang-Dae Park¹, Ji-Suk Gu¹,
Dae-Geun Kim², and Se-Hyeong Jeon³

¹*Department of Energy Systems, Korea Institute of Machinery & Materials, Daejeon, Korea*

²*Department of R&D Center, Poonglim Co., Ltd, Seoul, Korea*

³*Innotems Innovation Systems Co., Daejeon, Korea*

**Corresponding author (bzoo77@kimm.re.kr)*

ABSTRACT: Though vacuum suction pads are able to fasten items of working equipment such as gondolas easily and without causing damage to a building's outer wall, their necessary suction force should be designed by considering various conditions such as wind force, the loads of each item of working equipment, and suction capacity. Suction force is changed by the internal vacuum pressure of pads, and the materials and shapes of an outer wall's surface have a considerable influence on vacuum pressure.

In this study, we measured the vacuum suction force of pads on walls configured of various materials and shapes.

Keywords: *Vacuum Suction Force, Suction Pads, Vertical Outer Wall, Wall Shape, Gondola, High-rise Building*

1. INTRODUCTION

The outer walls of high-rise buildings are made of various materials such as steel, red block, marble, glass, and so forth, and their surfaces can contain many grooves of irregular shapes and sizes. Table 1 presents the diverse materials used in the outer walls of buildings, as reported in previous studies^[1]. The outer walls of high-rise buildings require regular maintenance including cleaning and painting. Gondola systems are used to carry on platforms the workers who conduct maintenance work on the outer walls of high-rise buildings. However, for super-high-rise buildings, i.e., higher than 30 stories, it is very difficult to perform such work on their outer walls using a gondola due to external disturbances including squalls. To perform this kind of work on outer walls using gondolas, considerable attachment force (to the wall) is required, taking into consideration the external loads and work loads, so vacuum pads are used to apply the force.

Table 1. Various outer wall materials

Type	Materials
A	Wood, stone, concrete, red block, glass, ceramic, plastic, fiber, metal, paper
B	Stone, block, tile, glass
C	Aluminum composite panel, stone, porcelain enamel panel, red block, cement

Dong Gwang L., et al. developed and tested a robot system using vacuum suction technology for cleaning the window panes of a building's outer walls^[2]. Kun Chan S., et al. designed a suction unit for a robot system which can climb up irregular vertical surfaces^[3]. Siyoul J conducted a study on the design of a vacuum suction pad which can provide a uniform contact shape in large-scale imprinting^[4]. However, robots traveling on vertical walls have limitations in terms of the shape of the walls and their adhesive force^[5-7]. Therefore, the vacuum suction ability with the various wall shapes should be evaluated and applied in the outer wall work system.

In this paper, a testing apparatus is developed to test the maximum adhesive forces of suction pads on various vertical wall surfaces according to pressure change. In addition, the vacuum pressure according to the change of pressure was measured for comparison with the adhesive forces required for safe working on various walls.

2. TEST EQUIPMENT

2.1. TEST EQUIPMENT SPECIFICATIONS

Fig. 2 shows the test equipment fabricated to measure the suction force on various vertical walls. A regulator was provided to maintain a constant pressure to obtain a constant suction force with an ejector-type suction pad (300 mm x 130 mm). The vertical and horizontal forces were measured using load cells which can measure up to 200 N of tensile and compressive forces. The pneumatic cylinder was a reciprocating cylinder which can travel bi-directionally. Fig. 1 shows the design drawing of a sliding block which can apply vertical and horizontal forces simultaneously. The sliding block was used to minimize interference between the two axes. The measurement data were collected using LabVIEW. Table 2 presents the specifications of the sub-components of the test equipment.

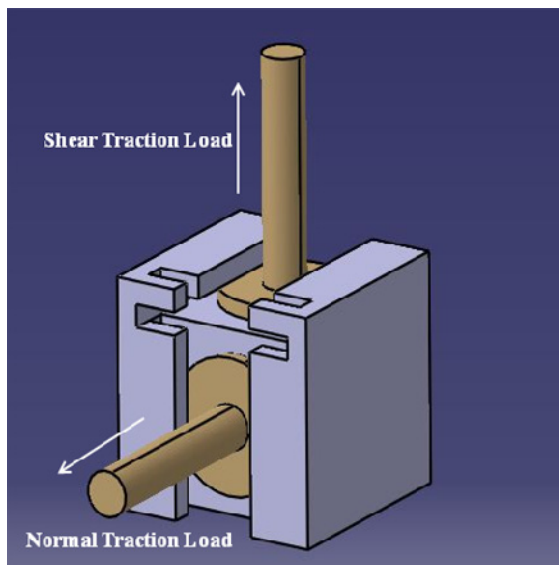


Fig. 1 Sliding block

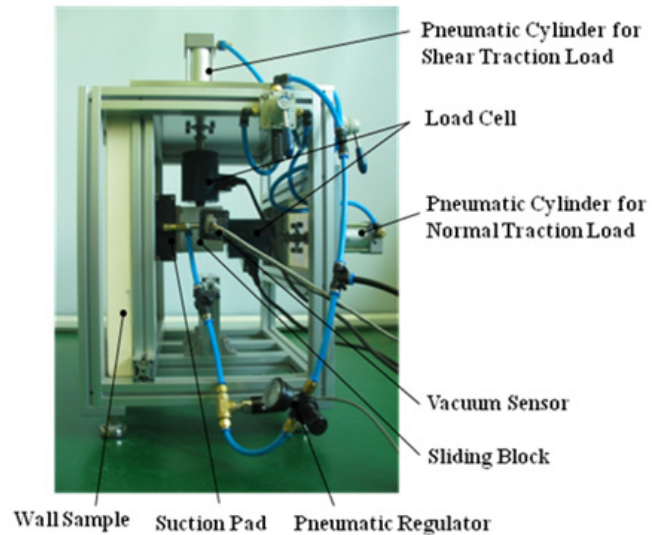


Fig. 2 Vacuum attachment device

Table 2. Specifications of the sub-components

Contents	Specifications
Wall type	Shape: flat surface
Load cell	Range: max. 200 N
Vacuum sensor	-Range: $10^{-3} \sim 10^3$ Torr -Accuracy: 0.1 % of indicated decade
Pneumatic cylinder	Max pressure : 1 MPa
Compressor	Max. pressure: 1 MPa
DAQ	Model: NI SCXI 1520(8 ch)

2.2. CONFIGURATION OF VERTICAL WALLS

To simulate the various wall configurations of high-rise buildings, four types of wall samples - including Flat, Step, Rib, and Embossing - were prepared. To conduct the tests under the same conditions as those to which the outer walls of a general high-rise building are subject, the wall samples were fabricated with concrete in the said configurations.





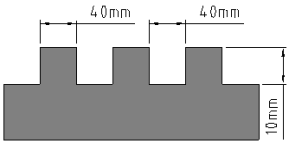
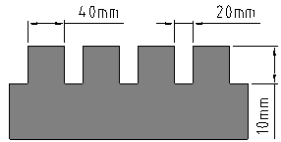

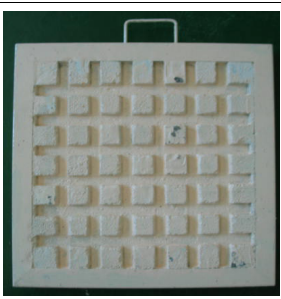
2.3. FEATURES OF SUCTION PAD

The suction pad used in this study was based on the ejector principle, whereby the air inside the pad is removed by the ejection of compressed air. Ejectors are used to suck

up and discharge, transfer or mix gases, liquids or powders. A multi-step nozzle-type VMECA Vacuum cartridge was inserted to maintain constant vacuum pressure even under low and irregular input pressure. The size of the suction pad was 300 mm x 130 mm and its cross-section 390 cm². The suction pad was made of flexible sealing foam with multiple holes measuring 12 mm in diameter and 20 mm in depth. The suction pad, which could be attached to the irregular surfaces of vertical walls, had a maximum relative vacuum pressure of 555 mmHg. Fig. 3 shows the structure of the vacuum suction pad in this study.

perpendicularly using the cylinder, and the maximum attachment forces of the vacuum suction pad were measured according to surface shapes. Fig. 4 shows the maximum attachment forces according to the shapes of the walls and compressed air pressure. Tables 4~7 present the vacuum pressure and maximum attachment forces of the pad according to air pressure.

Table 3. Shapes of the outer wall samples

Flat type	Step type
	
	
Rib type	Embossing type
	
	

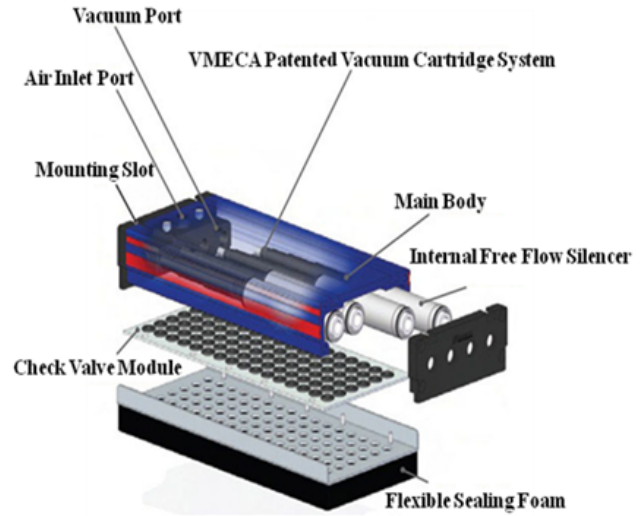


Fig. 3 View of the disassembled vacuum pad

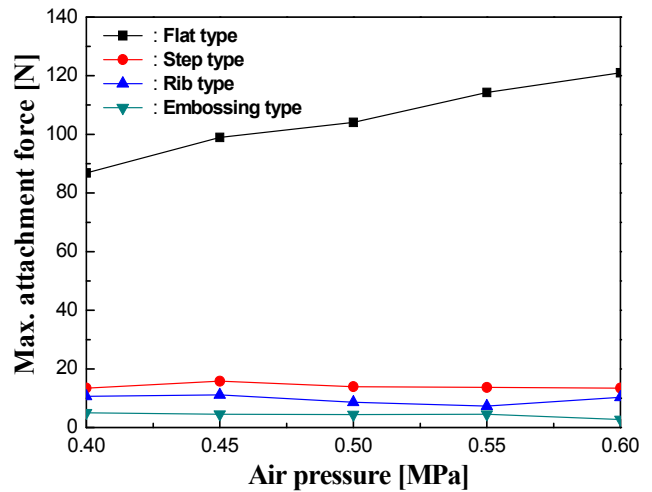


Fig.4 Results graph of max. attachment force with air pressure

3. TEST RESULTS

The pad was attached to the wall's surface and pulled

Table 4. Test results of flat-type sample

Input Pressure [MPa]	Vacuum Pressure (-mmHg)	Max. Attachment Force (N)
0.4	355	86.87
0.45	421	98.99
0.5	500	104.12
0.55	585	114.27
0.6	605	120.97

Table 5. Test results of step-type sample

Input Pressure [MPa]	Vacuum Pressure (-mmHg)	Max. Attachment Force (N)
0.4	232	13.44
0.45	259	15.81
0.5	259	13.94
0.55	280	13.64
0.6	245	13.44

Table 6. Test results of rib-type sample

Input Pressure [MPa]	Vacuum Pressure (-mmHg)	Max. Attachment Force (N)
0.4	223	10.68
0.45	242	11.18
0.5	254	8.61
0.55	222	7.33
0.6	235	10.29

Table 7. Test results of embossing-type sample

Input Pressure [MPa]	Vacuum Pressure (-mmHg)	Max. Attachment Force (N)
0.4	209	4.99
0.45	215	4.5
0.5	216	4.4
0.55	213	4.51
0.6	216	2.72

The results of the test showed that the ranges of vacuum pressure and attachment forces on the flat-type wall were 355~605 mmHg and 86.9~121 N, respectively. Those observed for the other types were as follows: 1) step-type: 232~280 mmHg and 13.4~15.8 N; 2) rib-type: 222~254 mmHg and 7.3~11.2 N; and 3) embossing-type 209~216 mmHg and 2.7~5 N.

On the flat-type wall, the vacuum pressure and attachment force increased proportionally with the increase in the amount of input air pressure. However, for the step-type, while the maximum vacuum pressure was 280 mmHg, the maximum attachment force was 15.6 N at 259 mmHg of vacuum pressure; for the rib-type, while the maximum vacuum pressure was 254 mmHg at 0.5 MPa of air pressure, the maximum attachment force was 11 N at 242 mmHg of vacuum pressure; and for the embossing-type wall, the maximum attachment force was obtained at the lowest vacuum pressure of 209 mmHg.

3. CONCLUSIONS

In this study, testing equipment was fabricated to test and measure the attachment performance of a vacuum suction pad on various configurations of wall surface, i.e., flat, step, rib, and embossing types, formed with concrete material. Since the suction pad was based on the ejector principle, the higher the air pressure, the higher the vacuum pressure.

The test results showed that, while the attachment force on the flat-type wall was 86.9 N or above, that on the other types of wall were 0.2 N or less, showing that the performance of the suction pad decreases greatly on irregular wall surfaces. On the step, rib, and embossing types of surfaces, the vacuum pressure in the pad did not increase while the air pressure was being increased, but showed irregular values within a certain range. The attachment performance became increasingly inferior in the flat, step, rib, and embossing types of wall configuration in that order.

The test results show that the performance of the suction pad depends more on the configuration of a wall's surface than on the attachment force generated by air pressure. As such, it could be concluded that the performance of the vacuum suction pad is reliable on flat surfaces, but not on stepped, ribbed or embossed surfaces due to the loss of

vacuum pressure via their irregular grooves.

The results obtained in this study are expected to be applicable to the design of the suction pads used in wall-climbing robots or wall-work systems including gondolas.

ACKNOWLEDGEMENTS

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REFERENCES

- [1] Ji-Seok, J. et al, "A Study on Choice of the Type of Curtain Wall and the Exterior Material according to Commercial Building Images by using the AHP", Vol. 22(11), pp.89-96, 2006.
- [2] Dong-Kwang L. et al, "An instrument of building an outer-wall window-cleaning robot and controller layout using vacuum adsorption technology", pp. 259-260, 2007.
- [3] Kunchan S. et al, "Design of an attachment device for robotic systems that climb rugged vertical surfaces", *KSPE*, pp. 99-100, 2007.
- [4] Siyoul Jang, "A study on the enhancement of uniform contact technology for large-scale imprinting with the design of a vacuum gripping pad", *Journal of the KSTLE*, Vol.24(6), pp. 623-331, 2008.
- [5] M. Elliot, W. Norris, J.Xiao, "City-Climber: A new generation of wall-climbing robots", *Proceedings of the 2007 IEEE International Conference on Robotics and Automation*, 2007.
- [6] S. Hirose, A. Nagakubo, R. Toyama, "A machine that can walk and climb on floors, walls and ceilings", *International Conference on Advanced Robotics*, Vol. 1, pp. 753-758, 1991.
- [7] Alan T. et al, "Scaling hard vertical surfaces with

compliant microspine arrays", *The International Journal of Robotic Research*, Vol. 25, pp. 1165-1179, 2006.